

Numerical Analysis of the Electrical Potential Calculation in a Transversely Isotropic Media

Sri Mardiyati *, T. Basyarudin and Heru Suhartanto

Faculty of Computer Sciences, University of Indonesia, Kampus Depok, Indonesia 16424

*To whom correspondence should be addressed. E-mail: sri_mardiyati@hotmail.com

Received 16 October 2006

<http://dx.doi.org/10.11113/mjfas.v2n1-2.19>

ABSTRACT

The electrical potential due to a point source of current supplied at the surface of a transversely isotropic medium is calculated using a finite element formulation. The finite and infinite elements are applied to calculate the potential for arbitrary electrical conductivity profiles. The accuracy of the scheme is checked against results obtainable using Chave's algorithm.

Transversely isotropic | transverse conductivity | vertical conductivity | direct current | electrical potential | finite element | infinite element |

1. Introduction

The analytical solution for the electrical potential in transversely isotropic earth is represented as an integral equation form. Some authors calculated the electrical potential by solving the integral equation numerically. Sampaio [6] investigated cases in an isotropic medium. Stoyer and Wait [8] analyzed a two-layer model of isotropic medium, where the lower layer has an exponentially varying conductivity. Sato and Sampaio [7] considered a half-space whose resistivity varies as the power of an expression depending linearly on depth. However, their methods are limited to specific forms of conductivity.

In this paper, the electrical potential $\varphi(r, z)$ in transversely isotropic media is chosen as a model. The potential resulting from a single current electrode located at the origin of a cylindrical coordinate system, which is axially symmetry satisfies a Boundary Value Problem (BVP) which consists of a partial differential equation:

$$\sigma_l \left(\frac{\partial^2 \phi}{\partial r^2} + \frac{1}{z} \frac{\partial \phi}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma_v \frac{\partial \phi}{\partial z} \right) = 0 \quad (1.1)$$

and two boundary conditions, those are:

(i) The vertical component of the current density must be zero at ground surface, this satisfies

$$\sigma_v(0) \frac{\partial \phi}{\partial z}(r,0) = \frac{1}{2\pi} \frac{\delta(r)}{r} \quad (1.2)$$

(ii) The electrical potential must approximate to zero at infinite distance, this satisfies

$$\phi(r,z) \rightarrow 0 \text{ as } \sqrt{r^2 + z^2} \rightarrow \infty \quad (1.3)$$

where σ_l is the conductivity in horizontal directions and σ_v is the conductivity in vertical current flow.

A finite element scheme is developed to solve this BVP for any form of conductivity profile in a medium. The basic steps involved in solving this method are:

- (1) The formulation of a variational statement with an appropriate space of admissible function identified.
- (2) The constructions of an approximation of the variational BVP on a finite dimensional subspace H^h .
- (3) The construction of a finite element mesh and piecewise-polynomial basis functions defined on the mesh.
- (4) Solving the system of equations.

The first step of finite element method will be shown on the following section.

2. Variational Statement of the Boundary Value Problem

The equation (1.1) can be written as follows:

$$\frac{1}{r} \frac{\partial}{\partial r} [r \sigma_l \frac{\partial \phi}{\partial r}] + \frac{\partial}{\partial z} [\sigma_v \frac{\partial \phi}{\partial z}] = 0 \quad (2.4)$$

In a cylindrical coordinate system which is axially symmetry, if $\bar{F} = [F_1, F_2]$ then the divergence of \bar{F} becomes:

$$\nabla \cdot \bar{F} = \frac{1}{r} \frac{\partial}{\partial r} [r F_1] + \frac{\partial}{\partial z} [F_2]$$

Applying the divergence of \bar{F} into equation (2.4), the BVP will consist of an equation:

$$\nabla \cdot \bar{F} = 0 \text{ where } F_1 = \sigma_l \frac{\partial \phi}{\partial r} \text{ and } F_2 = \sigma_v \frac{\partial \phi}{\partial z} \quad (2.5)$$

and the boundary conditions (1.2) and (1.3). The total weight residual error of equation (2.5) over a region Ω (see Figure 1) needs to be zero, that is:

$$\int_{\Omega} w(\nabla \cdot \bar{F}) d\Omega = \int_{\Omega} [\nabla \cdot w\bar{F} - \bar{F} \cdot \nabla w] d\Omega = \int_{\partial\Omega} w\bar{F} \cdot \bar{n} ds - \int_{\Omega} \bar{F} \cdot \nabla w d\Omega \quad (2.6)$$

where \bar{n} is an orthogonal vector to the boundary.

The integral on the boundary is calculated on three subregions of $\partial\Omega$, those are:

$$\partial\Omega_1 = z = 0, \partial\Omega_2 = r = 0 \text{ and } \partial\Omega_3 = \sqrt{r^2 + z^2} \rightarrow \infty$$

Now consider:

$$\int_{\partial\Omega} w\bar{F} \cdot \bar{n} ds = \int_{\partial\Omega_1} w\bar{F} \cdot \bar{n} ds + \int_{\partial\Omega_2} w\bar{F} \cdot \bar{n} ds + \int_{\partial\Omega_3} w\bar{F} \cdot \bar{n} ds$$

I

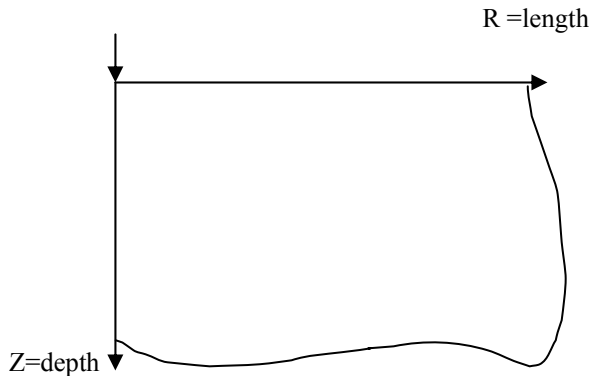


Figure 1: The domain Ω

On the boundary $\partial\Omega_1$ we have:

$$\int_{\partial\Omega_1} w \bar{F} \cdot \bar{n} \, ds = \int_{\partial\Omega_1} w \sigma_v \frac{\partial \phi}{\partial z} 2\pi r \, dr = \int_{\partial\Omega_1} -I w(r,0) \delta(r) \, dr = -I w(0,0) \tag{2.7}$$

On the boundary $\partial\Omega_2$, the boundary condition (1.1) is applied and the following result is obtained by choosing $w = 0$ on $\partial\Omega_2$:

$$\int_{\partial\Omega_2} w \bar{F} \cdot \bar{n} \, ds = \int_{\partial\Omega_2} w \sigma_l \frac{\partial \phi}{\partial r} 2\pi r \, dr = 0 \tag{2.8}$$

On the boundary $\partial\Omega_3$, $w = 0$ is chosen to obtain the following result:

$$\int_{\partial\Omega_3} w \bar{F} \cdot \bar{n} \, ds = 0 \tag{2.9}$$

By adding the results (2.7), (2.8) and (2.9), the integral on the boundary becomes:

$$\int_{\partial\Omega} w \bar{F} \cdot \bar{n} \, ds = -I w(0,0) \tag{2.10}$$

with weight function w is chosen such that $w=0$ on $\partial\Omega_2$ and $\partial\Omega_3$.

The integral in the domain Ω is obtained as follow:

$$\int_{\Omega} \bar{F} \cdot \nabla w \, d\Omega = \int_{\Omega} [F_1, F_2] \left[\frac{\partial w}{\partial r} \bar{e}_r + \frac{\partial w}{\partial z} \bar{e}_z \right] d\Omega = \int_{\Omega} \left[\sigma_l \frac{\partial \phi}{\partial r} \frac{\partial w}{\partial r} + \sigma_v \frac{\partial \phi}{\partial z} \frac{\partial w}{\partial z} \right] 2\pi r \, dr \, dz \tag{2.11}$$

Combining the equation (2.10) and (2.11), the total weight residual error over region Ω becomes:

$$\int_{\Omega} w(\nabla \cdot \bar{w}) \, d\Omega = -I w(0,0) - \int_{\Omega} \left[\sigma_l \frac{\partial \phi}{\partial r} \frac{\partial w}{\partial r} + \sigma_v \frac{\partial \phi}{\partial z} \frac{\partial w}{\partial z} \right] 2\pi r \, dr \, dz = 0$$

Atau:

$$\int_{\Omega} \left[\sigma_l \frac{\partial \phi}{\partial r} \frac{\partial w}{\partial r} + \sigma_v \frac{\partial \phi}{\partial z} \frac{\partial w}{\partial z} \right] r \, dr \, dz = \frac{-I}{2\pi} w(0,0) \tag{2.12}$$

Hence the variational of the BVP can now be stated concisely in the following term: find $\phi(r, z) \in H^1(\Omega)$ such that:

$$\int_{\Omega} \left[\sigma_l \frac{\partial \phi}{\partial r} \frac{\partial w}{\partial r} + \sigma_v \frac{\partial \phi}{\partial z} \frac{\partial w}{\partial z} \right] r dr dz = \frac{-I}{2\pi} w(0,0) \quad \forall w(r, z) \in H^1(\Omega) \quad (2.13)$$

where $w(r, z)$ is a weight function and the space of admissible function $H^1(\Omega)$ is given by:

$$H^1(\Omega) = \left\{ v \mid v, \frac{\partial v}{\partial r}, \frac{\partial v}{\partial z} \text{ are square integrable and } v(r, z) = 0 \text{ if } \sqrt{r^2 + z^2} \rightarrow \infty \right\} \quad (2.14)$$

3. The Galerkin Approximation

A Galerkin approximation for solution ϕ is obtained by posing the variational problem on a finite dimensional subspace H^h of admissible function $H^1(\Omega)$ and the weight function chosen as a function in H^h . Specifically, we seek $\phi_h \in H^h$ such that

$$\int_{\Omega} \left[\sigma_l \frac{\partial \phi_h}{\partial r} \frac{\partial w_h}{\partial r} + \sigma_v \frac{\partial \phi_h}{\partial z} \frac{\partial w_h}{\partial z} \right] r dr dz = \frac{-I}{2\pi} w_h(0,0) \quad (3.15)$$

Let $\{\chi_i(r, z)\}_{i=1}^N$ be the basis functions of H^h , then ϕ_h and w_h can be represented as a linear combination of the basis functions:

$$\phi_h = \sum_{j=1}^N \alpha_j \chi_j(r, z) \quad \text{and} \quad w_h = \sum_{i=1}^N \beta_i \chi_i(r, z) \quad (3.16)$$

If the function w_h in (3.16) is substituted into equation (3.15), then the following result is obtained:

For the left hand side of (3.18) we have

$$\int_{\Omega} \left[\sigma_l \frac{\partial \phi_h}{\partial r} \sum_{i=1}^N \beta_i \frac{\partial \chi_i}{\partial r} + \sigma_v \frac{\partial \phi_h}{\partial z} \sum_{i=1}^N \beta_i \frac{\partial \chi_i}{\partial z} \right] r dr dz = \frac{-I}{2\pi} \sum_{i=1}^N \beta_i \chi_i(0,0)$$

or

$$\sum_{i=1}^N \int_{\Omega} \left[\sigma_l \frac{\partial \phi_h}{\partial r} \frac{\partial \chi_i}{\partial r} + \sigma_v \frac{\partial \phi_h}{\partial z} \frac{\partial \chi_i}{\partial z} \right] \beta_i r dr dz = \frac{-I}{2\pi} \sum_{i=1}^N \beta_i \chi_i(0,0) \quad (3.17)$$

Because β_i are arbitrary, the equation (3.17) represents N equations to be satisfied by the α_i defining ϕ_h rather than the single equation. By choosing $\beta_i = 1, \beta_k = 0 \quad \forall k \neq i$ and $\forall i$, β_i is substituted into equation (3.17) then the following equation is obtained:

$$\int_{\Omega} \left[\sigma_l \frac{\partial \phi_h}{\partial r} \frac{\partial \chi_i}{\partial r} + \sigma_v \frac{\partial \phi_h}{\partial z} \frac{\partial \chi_i}{\partial z} \right] r dr dz = \frac{-I}{2\pi} \chi_i(0,0) \quad \text{for } i = 1, 2, \dots, N$$

The function $\phi_h = \sum_{j=1}^N \alpha_j \chi_j(r, z)$ is substituted into above equation and we get:

$$\sum_{j=1}^N \int_{\Omega} \left[\sigma_l \frac{\partial \chi_j}{\partial r} \frac{\partial \chi_i}{\partial r} + \sigma_v \frac{\partial \chi_j}{\partial z} \frac{\partial \chi_i}{\partial z} \alpha_j r dr dz \right] = \frac{-I}{2\pi} \chi_i(0,0) \quad \text{for } i=1,2,\dots,N$$

Now, we arrive at the system of N linear equation with N unknown α_j as follows:

$$\sum_{j=1}^N K_{ij} \alpha_j = F_i \quad \text{for } i=1,2,\dots,N \text{ or } K \alpha = F \tag{3.18}$$

Where

$$K_{ij} = \int_{\Omega} \left[\sigma_l \frac{\partial \chi_j}{\partial r} \frac{\partial \chi_i}{\partial r} + \sigma_v \frac{\partial \chi_j}{\partial z} \frac{\partial \chi_i}{\partial z} r dr dz \right] \text{ and } F_i = \frac{-I}{2\pi} \chi_i(0,0) \tag{3.19}$$

The K is called the Stiffness matrix order ($N \times N$), α is unknown and F is called load vector. Matrix K in equation (3.18) is invertible because $\{\chi_i(r, z)\}_{i=1}^N$ is linearly independent, so the coefficient α_j will be unique. Therefore the Galerkin's approximation ϕ_h of the solution ϕ is on the form:

$$\phi_h = \sum_{j=1}^N \alpha_j \chi_j(r, z) \quad \text{where } \alpha_j \text{ is the solution of the linear system (3.18) and } \{\chi_i(r, z)\}_{i=1}^N \text{ is the basis function of } H^h.$$

4. Finite Element Method

The FEM provides a general and systematic technique for construction the basis functions $\{\chi_i(r, z)\}_{i=1}^N$ for the Galerkin's approximation. The procedure is started by divided Ω into two regions, those are a finite element mesh: $\Omega_f = \{(r, z) | 0 \leq r \leq L \text{ and } 0 \leq z \leq D\}$ and an infinite element mesh $\Omega_i = \{(r, z) | r > L, z > D\}$

The finite element mesh Ω_f and Ω_i is generated by mapping a nine-point isoparametric master element $\bar{\Omega}$ with coordinate (ξ, η) in Cartesian and the origin $(0, 0)$ is located at the center of $\bar{\Omega}$. The master element is transformed into the $r z$ -plane by using the following coordinate transformation:

$$r = \sum_{i=0}^8 r_i \psi_i(\xi, \eta) \quad \text{and} \quad z = \sum_{j=0}^8 z_j \psi_j(\xi, \eta)$$

where $(r_i, z_i), i=1,2,\dots,N$ are nodal points in Ω_f and $\psi_j, j=1,2,\dots,N$ is the set of master element shape functions (see [2]):

$$\begin{aligned} \psi_0(\xi, \eta) &= \frac{1}{4}(\xi^2 - \xi)(\eta^2 - \eta) & \psi_1(\xi, \eta) &= \frac{1}{2}(1 - \xi^2)(\eta^2 - \eta) & \psi_2(\xi, \eta) &= \frac{1}{4}(\xi^2 + \xi)(\eta^2 - \eta) \\ \psi_3(\xi, \eta) &= \frac{1}{2}(\xi^2 - \xi)(1 - \eta^2) & \psi_4(\xi, \eta) &= (1 - \xi^2)(1 - \eta^2) & \psi_5(\xi, \eta) &= \frac{1}{2}(\xi^2 + \xi)(1 - \eta^2) \\ \psi_6(\xi, \eta) &= \frac{1}{4}(\xi^2 - \xi)(\eta^2 + \eta) & \psi_7(\xi, \eta) &= \frac{1}{2}(1 - \xi^2)(\eta^2 + \eta) & \psi_8(\xi, \eta) &= \frac{1}{4}(\xi^2 + \xi)(\eta^2 + \eta) \end{aligned}$$

For the region Ω_i , the method as outlined in Zienkiewicz [9] is used for mapping the master element to infinite element with the following element shape functions:

$$\tau_0(\xi, \eta) = (\eta - \eta^2) \left(\frac{\xi}{1 - \xi} \right), \quad \tau_1(\xi, \eta) = \frac{1}{2}(\eta - \eta^2) \left(1 + \frac{2\xi}{1 - \xi} \right), \quad \tau_2(\xi, \eta) = 2(1 - \eta^2) \left(\frac{\xi}{1 - \xi} \right)$$

$$\tau_3(\xi, \eta) = (1 - \eta^2) \left(1 + \frac{2\xi}{1-\xi}\right), \quad \tau_4(\xi, \eta) = (\eta + \eta^2) \left(\frac{\xi}{1-\xi}\right), \quad \tau_5(\xi, \eta) = \frac{1}{2}(\eta + \eta^2) \left(1 + \frac{2\xi}{1-\xi}\right)$$

and the coordinate transformation is as follows:

$$r = \sum_{i=0}^5 r_i \tau_i(\xi, \eta) \quad \text{and} \quad z = \sum_{j=0}^5 z_j \tau_j(\xi, \eta) \quad \text{where } (r_i, z_i), i=1,2,\dots,N \text{ are nodal points in } \Omega_i.$$

The integral (3.19) is evaluated by using The Gaussian Quadrature formula of order 3 in every element. The stiffness matrix K is constructed based on these results and the linear system (3.18) is solved to obtain the value of the electrical potential in every nodal point.

4.1 Interpolation Error

The actual solution φ of the boundary value problem will be interpolated by a finite element representation φ_h which contains complete polynomial of degree 2. The interpolation error function $E = \varphi - \varphi_h$ on $\Omega_e = \{(r, z) | r_i < r < r_{i+1}, z_i < z < z_{i+1}\}$ can be expanded in a Taylor series about any interior point $(\bar{r}, \bar{z}) \in \Omega_e$ as follow (see [5]):

$$E(r, z) = E(\bar{r}, \bar{z}) + [(r - \bar{r})E_r(\bar{r}, \bar{z}) + (z - \bar{z})E_z(\bar{r}, \bar{z})] + \frac{1}{2}[(r - \bar{r})^2 E_{rr}(r_0, z_0) + 2(z - \bar{z})(r - \bar{r})E_{rz}(r_0, z_0) + (z - \bar{z})^2 E_{zz}(r_0, z_0)]$$

where r_0 is between r and \bar{r} , z_0 is between z and \bar{z} . Since φ_h is interpolation of φ then E is zero at end point (r_e, z_e) where $r_e = r_i$ or $r_e = r_{i+1}$ and $z_e = z_i$ or $z_e = z_{i+1}$. If point (\bar{r}, \bar{z}) is selected to be a point which make $|E|$ is maximum, then $E_r(\bar{r}, \bar{z}) = 0$, $E_z(\bar{r}, \bar{z}) = 0$. The error function E becomes:

$$E(r, z) = E(\bar{r}, \bar{z}) + \frac{1}{2}[(r - \bar{r})^2 E_{rr}(r_0, z_0) + 2(z - \bar{z})(r - \bar{r})E_{rz}(r_0, z_0) + (z - \bar{z})^2 E_{zz}(r_0, z_0)]$$

If we set (r, z) as end point (r_i, z_i) or (r_{i+1}, z_{i+1}) whichever is closer to (\bar{r}, \bar{z}) , say (r_i, z_i) then $E(r_i, z_i) = 0$. So the following result is obtained:

$$E(\bar{r}, \bar{z}) = -\frac{1}{2}[(r_i - \bar{r})^2 E_{rr}(r_0, z_0) + 2(z_i - \bar{z})(r_i - \bar{r})E_{rz}(r_0, z_0) + (z_i - \bar{z})^2 E_{zz}(r_0, z_0)]$$

or

$$|E(\bar{r}, \bar{z})| \leq \frac{1}{2}[(r_i - \bar{r})^2 |E_{rr}(r_0, z_0)| + 2(z_i - \bar{z})(r_i - \bar{r}) |E_{rz}(r_0, z_0)| + (z_i - \bar{z})^2 |E_{zz}(r_0, z_0)|]$$

Assume that h_e is the largest distance between two points in Ω_e , then $|r_i - \bar{r}| \leq \frac{h_e}{2}$ and $|z_i - \bar{z}| \leq \frac{h_e}{2}$ or the error bound becomes:

$$|E(\bar{r}, \bar{z})| \leq \frac{h_e^2}{8} [|E_{rr}(r_0, z_0)| + 2|E_{rz}(r_0, z_0)| + |E_{zz}(r_0, z_0)|]$$

Finally, $E = \phi - \phi_h$ implies $E'' = \phi'' - \phi_h'' = \phi''$ within Ω_e . If this condition is applied and

$C = \max_{(r,z) \in \Omega_e} |\phi''(r,z)|$ is assumed then we arrive on the following result: $|E(\bar{r}, \bar{z})| \leq C \frac{h_e^2}{2}$. So the

interpolation error satisfies: $\|\phi - \phi_h\|_{\infty, \Omega_e} = \max_{(r,z) \in \Omega_e} |\phi(r,z) - \phi_h(r,z)| \leq C_1 h_e^2$, where $C_1 = \frac{C}{2}$

and h_e is the largest distance between two points in Ω_e . Similarly, $\left\| \frac{\partial \phi}{\partial r} - \frac{\partial \phi_h}{\partial r} \right\|_{\infty, \Omega_e} \leq C_2 h_e$ and

$\left\| \frac{\partial \phi}{\partial z} - \frac{\partial \phi_h}{\partial z} \right\|_{\infty, \Omega_e} \leq C_3 h_e$. If the norm on the H^1_{Ω} is defined as follows $\|\phi\| = \left[\int_{\Omega} \left(\frac{\partial \phi}{\partial r} \right)^2 + \left(\frac{\partial \phi}{\partial z} \right)^2 dr dz \right]^{\frac{1}{2}}$ then

the interpolation error, measured in H^1_{Ω} -norm becomes: $\|E\|_{\Omega} \leq C_4 h^2$, for h is the largest distance between two points in every element Ω or ϕ converge to ϕ_h with rate of convergence h^2 .

4.2 The Accuracy of the Finite Element Approximation

The global matrix K in linear system (3.18) is a sparse matrix. If K is stored in a 2-dimension array, it is leading to an extravagant waste of computer storage and computer time. Therefore, the storage of K is modified by storing the non zero entries in K into an one dimensional array. If K is stored in a 2-dimension array, the code can only solve a problem in a mesh with 3600 nodes, but if K is stored in a one-dimension array, then the code can solve it for a mesh with 14400 nodes. By increased the number of nodes, the accuracy of the results will be improved. Tables 1, 2, 3 show the potential values and the enhancement of the relative error on the surface for distance 10 units, 20 units, 40 units and Table 4, 5, 6 show for distance 15 units, 30 units, and 60 units. The results are compared with the results obtained by using Chave's algorithms. The largest relative error in the range shown is less than 3% for the node located around the source.

Table 1. The potential and the relative-error on the surface with $AB=10$ units and the conductivity $\sigma_v = 2e^{0.2z}$, $\sigma_l = 3e^{0.2z}$

R	V(Chaves)	The Potential			Relative-error		
		r=c=21	r=c=41	r=c=81	r=c=21	r=c=41	r=c=81
2	0.020209	0.024379	0.020613	0.020215	0.206351	0.019984	0.000280
3	0.011328	0.011672	0.011353	0.011328	0.030365	0.002182	0.000020
4	0.007243	0.007436	0.007245	0.007242	0.026719	0.000365	0.000039
5	0.004985	0.005002	0.004986	0.004985	0.003260	0.000076	0.000080
6	0.003599	0.003605	0.003599	0.003599	0.001748	0.000040	0.000123
7	0.002687	0.002683	0.002687	0.002687	0.001405	0.000130	0.000175
8	0.002057	0.002051	0.002056	0.002056	0.002852	0.000226	0.000240
9	0.001605	0.001598	0.001605	0.001605	0.004747	0.000348	0.000322
10	0.001272	0.001263	0.001272	0.001272	0.007439	0.000520	0.000427

Table 2. The potential and the relative-error on the surface with AB=20 units and the conductivity $\sigma_v = 2e^{0.2z}$, $\sigma_l = 3e^{0.2z}$

R	The Potential			Relative-error			
	V(Chaves)	r=c= 21	r=c=41	r=c=81	r=c=21	r=c=41	r=c=81
4	0.007243	0.009249	0.007442	0.007246	0.277064	0.027534	0.000428
6	0.003599	0.003782	0.003612	0.003600	0.050895	0.003516	0.000095
8	0.002057	0.002154	0.002058	0.002057	0.047005	0.000765	0.000041
10	0.001272	0.001283	0.001273	0.001272	0.008217	0.000308	0.000021
12	0.000828	0.000833	0.000829	0.000828	0.005631	0.000137	0.000009
14	0.000559	0.000559	0.000559	0.000559	0.000793	0.000011	0.000001
16	0.000388	0.000387	0.000388	0.000388	0.003795	0.000126	0.000009
18	0.000275	0.000273	0.000275	0.000275	0.008420	0.000325	0.000023
20	0.000198	0.000195	0.000198	0.000198	0.015671	0.000664	0.000048

Table 3. The potential and the relative-error on the surface with AB=40 units and the conductivity $\sigma_v = 2e^{0.2z}$, $\sigma_l = 3e^{0.2z}$

R	The Potential			Relative-error			
	V(Chaves)	r=c=21	r=c=41	r=c=81	r=c=21	r=c=41	r=c=81
8	0.002057	0.002989	0.002155	0.002058	0.453183	0.047914	0.000801
12	0.000828	0.000927	0.000835	0.000829	0.118960	0.008057	0.000233
16	0.000388	0.000437	0.000389	0.000388	0.125478	0.002379	0.000127
20	0.000198	0.000205	0.000199	0.000198	0.034969	0.001297	0.000084
24	0.000107	0.000111	0.000107	0.000107	0.031763	0.000894	0.000059
28	0.000060	0.000061	0.000060	0.000060	0.012119	0.000610	0.000039
32	0.000035	0.000035	0.000035	0.000035	0.006672	0.000273	0.000015
36	0.000021	0.000021	0.000021	0.000021	0.006423	0.000340	0.000030
40	0.000012	0.000012	0.000012	0.000012	0.030762	0.001766	0.000140

Table 4. The potential and the relative-error on the surface with AB=15 units and the conductivity $\sigma_v = 2e^{0.2z}$, $\sigma_l = 3e^{0.2z}$

R	The Potential			Relative-error			
	V(Chaves)	r=c=31	r=c=61	r=c=121	r=c=31	r=c=61	r=c=121
2	0.020209	0.024363	0.020613	0.020215	0.205562	0.020005	0.000301
3	0.011328	0.011656	0.011353	0.011329	0.028954	0.002219	0.000058
4	0.007243	0.007420	0.007246	0.007243	0.024507	0.000424	0.000022
5	0.004985	0.004985	0.004986	0.004985	0.000040	0.000164	0.000009
6	0.003599	0.003589	0.003599	0.003599	0.002712	0.000086	0.000004
7	0.002687	0.002667	0.002687	0.002687	0.007357	0.000048	0.000000
8	0.002057	0.002035	0.002057	0.002057	0.010548	0.000024	0.000003
9	0.001605	0.001582	0.001605	0.001605	0.014393	0.000006	0.000006
10	0.001272	0.001248	0.001272	0.001272	0.019079	0.000010	0.000009

Table 5. The potential and the relative-error on the surface with AB=30 and the conductivity $\sigma_v = 2e^{0.2z}$, $\sigma_l = 3e^{0.2z}$

R	The Potential			Relative-error			
	V(Chaves)	r=c=31	r=c=61	r=c=121	r=c=31	r=c=61	r=c=121
4	0.007243	0.009250	0.007442	0.007246	0.277155	0.027543	0.000429
6	0.003599	0.003783	0.003612	0.003600	0.051077	0.003535	0.000097
8	0.002057	0.002154	0.002058	0.002057	0.047324	0.000798	0.000044
10	0.001272	0.001283	0.001273	0.001272	0.008748	0.000363	0.000025
12	0.000828	0.000834	0.000829	0.000828	0.006498	0.000225	0.000016
14	0.000559	0.000560	0.000560	0.000559	0.000643	0.000155	0.000011
16	0.000388	0.000388	0.000388	0.000388	0.001329	0.000110	0.000008
18	0.000275	0.000274	0.000275	0.000275	0.003992	0.000075	0.000006
20	0.000198	0.000197	0.000198	0.000198	0.007287	0.000044	0.000004

Table 6. The potential and the relative-error on the surface with AB=60 units and the conductivity $\sigma_v = 2e^{0.2z}$, $\sigma_l = 3e^{0.2z}$

R	The Potential			Relative-error			
	V(Chaves)	r=c=31	r=c=61	r=c=121	r=c=31	r=c=61	r=c=121
4	0.007243	0.009465	0.009251	0.007442	0.306849	0.277318	0.027544
8	0.002057	0.002989	0.002155	0.002058	0.453223	0.047917	0.000801
12	0.000828	0.000927	0.000835	0.000829	0.119063	0.008065	0.000234
16	0.000388	0.000437	0.000389	0.000388	0.125717	0.002395	0.000129
20	0.000198	0.000205	0.000199	0.000198	0.035498	0.001333	0.000086
24	0.000107	0.000111	0.000107	0.000107	0.032936	0.000969	0.000065
28	0.000060	0.000061	0.000060	0.000060	0.014767	0.000775	0.000052
32	0.000035	0.000035	0.000035	0.000035	0.012853	0.000649	0.000044
36	0.000021	0.000021	0.000021	0.000021	0.008422	0.000558	0.000038
40	0.000012	0.000013	0.000013	0.000012	0.006259	0.000481	0.000033

5. Conclusion

The verification confirms the accuracy of the finite element code. Although in most practical problems only the potential on the surface of the earth is measurable, our scheme does give the potential at every node in the computational domain. Further research will investigate the application of the code to the inverse problem of determining various conductivity profiles based on surface measurements.

6. References

- [1] A. D. Chave, *Geophysics*, 48 (1983) 1671-1686.
- [2] E. B. Becker, G. F. Carey, J. T. Oden, ``Finite Elements, An Introduction``, Volume I, Prentice-Hall Inc, 1981.
- [3] F. S. Grant, G. F. West, ``Interpretation Theory in Applied Geophysics``, McGraw - Hill Book Company, 1965.
- [4] D. W. Oldenburg, *Geophysics* 43 (1978) 610-625.
- [5] R. L. Burden, J. D. Faires, ``Numerical Analysis'', [Brooks/Cole Publishing Company, 1997].
- [6] E. S. Sampaio, *Geophysical Prospecting* 24 (1976) 112-122.
- [7] H. K. Sato, E. S. Sampaio, *Geophysical Prospecting*, 28 (1980) 967 - 976.
- [8] C. H. Stoyer, J. R. Wait, *Geoexploration* 15 (1977) 11-18.
- [9] O. C. Zienkiewicz, R. L. Taylor, ``The Finite Element Method'', Fourth Edition, McGraw-Hill Book Company, 1994.